

# Direct Stiffness Method – Constraints

Simulation Methods in Acoustics

# Single Degree of Freedom Constraints – SDFC

Unconstrained system

$$\mathbf{K}\mathbf{u} = \mathbf{f} \quad (1)$$

Some Nodal displacement values are prescribed:

$$\mathbf{u}_c = \bar{\mathbf{u}} (= \mathbf{0}) \quad (2)$$

SDFC: Each constraint equation addresses 1 DOF

Partitioning:  $c$ : constrained,  $u$ : unconstrained

$$\begin{bmatrix} \mathbf{K}_{cc} & \mathbf{K}_{cu} \\ \mathbf{K}_{uc} & \mathbf{K}_{uu} \end{bmatrix} \begin{Bmatrix} \mathbf{u}_c = \bar{\mathbf{u}} \\ \mathbf{u}_u \end{Bmatrix} = \begin{Bmatrix} \mathbf{f}_c \\ \mathbf{f}_u \end{Bmatrix} \quad (3)$$

Reduced system for the unconstrained displacements:

$$\mathbf{K}_{uu}\mathbf{u}_u = \mathbf{f}_u - \mathbf{K}_{uc}\bar{\mathbf{u}} \quad (4)$$

# Multiple Degree of Freedom Constraints

Examples:

	canonical form
$u_1 = u_3$	$u_1 - u_3 = 0$
$u_1 = \frac{u_2 + u_3}{2}$	$u_1 - \frac{1}{2}u_2 - \frac{1}{2}u_3 = 0$

General canonical form:

$$\sum_i a_i u_i = 0 \quad (5)$$

Multiple ( $K$ ) constraint equations for  $N$  DOF

$$\mathbf{A}\mathbf{u} = \mathbf{0}, \quad \mathbf{A} \in \mathbb{R}^{K \times N} \quad (6)$$

Objective: Solve  $\mathbf{K}\mathbf{u} = \mathbf{f}$  so that  $\mathbf{A}\mathbf{u} = \mathbf{0}$  holds.

## MDFC – Master Slave Method

- ▶ Assume that  $\mathbf{A}$  contains  $K$  independent constraints:  
 $\text{rank}\mathbf{A} = K$
- ▶ Each constraint lowers the # unknowns by one
- ▶  $N - K$  master DOF
- ▶  $K$  slave DOF are completely determined by the master DOF

Partition the DOF so that  $\mathbf{A}_s$  is invertible

$$\begin{bmatrix} \mathbf{A}_m & \mathbf{A}_s \end{bmatrix} \begin{Bmatrix} \mathbf{u}_m \\ \mathbf{u}_s \end{Bmatrix} = \mathbf{0} \quad \rightarrow \quad \mathbf{u}_s = -\mathbf{A}_s^{-1}\mathbf{A}_m\mathbf{u}_m \quad (7)$$

Total - Master dependence

$$\mathbf{u} = \begin{Bmatrix} \mathbf{u}_m \\ \mathbf{u}_s \end{Bmatrix} = \begin{bmatrix} \mathbf{I} \\ -\mathbf{A}_s^{-1}\mathbf{A}_m \end{bmatrix} \mathbf{u}_m = \mathbf{T}\mathbf{u}_m \quad (8)$$

$$\mathbf{K}\mathbf{T}\mathbf{u}_m = \mathbf{f} \quad (9)$$

Final constrained  $N - K \times N - K$  system:

$$\mathbf{T}^T\mathbf{K}\mathbf{T}\mathbf{u}_m = \mathbf{T}^T\mathbf{f}, \quad \hat{\mathbf{K}}\mathbf{u}_m = \hat{\mathbf{f}} \quad (10)$$

## Master-Slave Method – Simple connections

Unconnected 1D system of two springs

$$\begin{bmatrix} K_1 & -K_1 & & & & \\ -K_1 & K_1 & & & & \\ & & K_2 & -K_2 & & \\ & & -K_2 & K_2 & & \\ & & & & & & \end{bmatrix} \begin{Bmatrix} u_1 \\ u_2 \\ u_3 \\ u_4 \end{Bmatrix} = \begin{Bmatrix} f_1 \\ f_2 \\ f_3 \\ f_4 \end{Bmatrix} \quad (11)$$

Constraint:  $u_2 = u_3$ . Slave:  $u_3$ , Masters:  $u_1, u_2, u_4$ .

$$\begin{Bmatrix} u_1 \\ u_2 \\ u_3 \\ u_4 \end{Bmatrix} = \begin{bmatrix} 1 & & & \\ & 1 & & \\ & & 1 & \\ & & & 1 \end{bmatrix} \begin{Bmatrix} u_1 \\ u_2 \\ u_4 \end{Bmatrix} \quad (12)$$

$$\mathbf{T}^T \mathbf{K} \mathbf{T} = \begin{bmatrix} K_1 & -K_1 & & \\ -K_1 & K_1 + K_2 & -K_2 & \\ & -K_2 & K_2 & \\ & & & \end{bmatrix}, \quad \mathbf{T}^T \mathbf{f} = \begin{Bmatrix} f_1 \\ f_2 + f_3 \\ f_4 \end{Bmatrix} \quad (13)$$

## Master Slave Method – Rigid body motion

- ▶ Slave nodes connected by a massless rigid body
- ▶ Master DOF: Displacements  $u_{x0}$ ,  $u_{y0}$  and rotation  $\theta_0$  around  $(x_0, y_0)$ :
- ▶ Displacement field of the rigid body

$$u_x(x, y) = u_{x0} - (y - y_0)\theta_0 \quad (14)$$

$$u_y(x, y) = u_{y0} + (x - x_0)\theta_0 \quad (15)$$

- ▶ Master-slave constraints for one slave node:

$$\mathbf{u}_s = \begin{bmatrix} 1 & & -(y - y_0) \\ & 1 & x - x_0 \end{bmatrix} \begin{Bmatrix} u_{x0} \\ u_{y0} \\ \theta_0 \end{Bmatrix} \quad (16)$$

## MDFC – The Penalty Method

$$\mathbf{K}\mathbf{u} = \mathbf{f}, \quad \mathbf{A}\mathbf{u} = \mathbf{0} \quad (17)$$

Example constraint:  $u_i = u_j \rightarrow u_i$  and  $u_j$  are rigidly connected

$$\begin{bmatrix} 1 & -1 \end{bmatrix} \begin{Bmatrix} u_i \\ u_j \end{Bmatrix} = 0 \quad (18)$$

Represent by a „very stiff“ spring:

$$w \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} \begin{Bmatrix} u_i \\ u_j \end{Bmatrix} = \begin{Bmatrix} 0 \\ 0 \end{Bmatrix}, \quad \mathbf{K}^P \mathbf{u} = \mathbf{0} \quad (19)$$

Solve

$$(\mathbf{K} + \mathbf{K}^P) \mathbf{u} = \mathbf{f}, \quad w \rightarrow \infty \quad (20)$$

Square rule:  $w = \max K \cdot 10^{d/2}$ , where the system precision is  $d$  decimal digits

## MDFC – The Penalty Method

General  $k$  –  $th$  constraint:  $\mathbf{a}_k \mathbf{u} = 0$

Create an element by premultiplying by  $\mathbf{a}_k^T$

$$\underbrace{w \mathbf{a}_k^T \mathbf{a}_k}_{\mathbf{K}_k^p} \mathbf{u} = \mathbf{0} \quad (21)$$

Final system of equations

$$\left( \mathbf{K} + \sum_k \mathbf{K}_k^p \right) \mathbf{u} = \mathbf{f} \quad (22)$$

or equivalently

$$(\mathbf{K} + w \mathbf{A}^T \mathbf{A}) \mathbf{u} = \mathbf{f} \quad (23)$$



# MDFC – The Lagrange Method

The  $K$  constraints are taken into account as an additional force term defined by  $K$  Lagrange multipliers  $\lambda$

$$\mathbf{K}\mathbf{u} = \mathbf{f} - \mathbf{A}^T\lambda \quad (24)$$

The total system to solve takes the form

$$\begin{bmatrix} \mathbf{K} & \mathbf{A}^T \\ \mathbf{A} & \mathbf{0} \end{bmatrix} \begin{Bmatrix} \mathbf{u} \\ \lambda \end{Bmatrix} = \begin{Bmatrix} \mathbf{f} \\ \mathbf{0} \end{Bmatrix}$$

Advantages

- ▶ Symmetric and sparse
- ▶ Lagrange multipliers obtained from the solution

Disadvantage:

- ▶ Bandwidth increases